BUEING

GPO PRICE \$	
CFSTI PRICE(S) \$	
Ha⊢ ≉ору (HC)	\$3.00
Microfiche (MF) _	

N 67-27508	
(ACCESSION NUMBER)	(THRU)
10	1
(PAGES)	(CODE)
CR-84474	
(NASA CR OR TMX OR AD NUMBER)	(CATEGORY)

AERO-SPACE DIVISION LAUNCH SYSTEMS BRANCH

DOCUMEN.	T NO. <u>T5-6556-10</u>		
VOLU	JMEOF	_	
TITLE EVALUATION OF MACHI	NE SEWN JOINTS FO	OR THE FLEXIB	E HEAT
SHIELD CURTAIN		**	
MODEL NO. SATURN	LV/S- CONTRACT N	O. <u>NAS8-5608</u>	*
			.86
ISSUE NO ISSUE	UED TO Accentif	ic of Jechn	ical Information
	,		- 1970 -
PREPARED BY J. Dexter	Van		12-6-66
SUPERVISED BY Tarmel	refor		12-20-66
APPROVED BY T. Kornell	M		12/30/66
APPROVED BY			
APPROVED BY			
APPROVED BY		·	

DISTRIBUTION

BOEING

E. L. Clark 5-7996 LS-92

J. N. Dexter 5-7996 LS-92

P. E. Oster 5-7354 LT-49

NASA

F. McDaniel R-P&VE-VNR
F. Uptagrafft R.P&VE-ME

Scientific and Technical Information Facility Marshall Space Flight Center Huntsville, Alabama (Attn: MS-1P)

Scientific and Technical Information Facility P.O. Box 33 College Park, Maryland 20740

CHANGE RECORD									
RFV	CEC-		PAGES		REV.	CECT		PAGES	
REV. SYM.	SECT.	REVISED	ADDED	DELETED	REV. SYM.	SECT.	REVISED	ADDED	DELETED
					·				
			·						:

REV. SYM.	BOEING NO. T5-6556-10
	PAGE

	REVISIONS			
REV. SYM	DESCRIPTION	DESCRIPTION DATE APPROV		
!**				
·				
		·		

REV. SYM	BOEING NO.	T5-6556-10
	PAGE	111
S-406-35-11 ORIG. 1/64	•	***

ABSTRACT

Joints in the wire reinforced asbestos and silica cloth plies of the 60B20508 flexible flame curtain assembly are currently being made by hand sewing. This investigation covers results of attempts to machine sew these joints. Results indicate that acceptable joints can be machine sewn in the silica cloth ply. Machine sewing was unsuccessful for the asbestos ply.

KEY WORDS

Asbestos Sewing

Flexible Flame Curtain

Machine Sewing

Sewing

Silica Cloth Sewing

| NO. T5-6556-10 | PAGE | iv

TABLE OF CONTENTS

	Distribution	i
	Change Record Page	ii
	Revisions Page	ii
	Abstract and Key Words	iv
	Table of Contents	v
1.0	Object	1
2.0	Background	1
3.0	Conclusions	1
4.0	Recommendations	1
5 0	Dranduras and Pagulta	1

1.0 OBJECT

The object of this investigation was to determine the feasibility of machine sewing the wire reinforced asbestos and silica cloth plies of the flexible heat shield curtain assembly.

BACKGROUND 2.0

The joints in the wire-reinforced asbestos and the silica cloth plies of the 60B20508 base heat shield curtain assembly are currently being sewn by hand. This test was conducted at the request of the Interstage and Heat Shield Group to determine the feasibility of machine sewing these joints. Should machine sewing prove to be feasible it could result in reducing manufacturing costs with a resulting cost savings.to Boeing.

3.0 CONCLUSIONS

The results of this investigation indicate that it is feasible to machine sew the joints in the silica cloth using type 12 Astroquartz sewing thread which meet the 60B20508 drawing and the 60B32053 acceptance specification requirements. The results also show that it is not feasible to machine sew the joints in the wire reinforced asbestos ply using the metallic filament thread, since none of the joints made during this investigation met the requirements of 60B32053.

RECOMMENDATIONS 4.0

It is recommended that the joints in the silica cloth ply of the 60B20508 curtain assembly be machine sewn using type 12 Astroquartz sewing thread.

It should be borne in mind that silica cloth has poor abrasion resistance, therefore provisions must be made to insure against abrasion or scuffing damage to the silica cloth during machine sewing.

5.0 PROCEDURES AND RESULTS

The wire reinforced asbestos and silica cloth plies of the 60B20508 flexible heat shield curtain assembly are currently being made using hand sewing While this does produce curtains of acceptable quality, it is relatively expensive. This program was performed at the request of the Interstage and Heat Shield Group to determine the feasibility of machine sewing the joints in these plies in order to effect a cost savings in the manufacture of the curtains. The request for this investigation specified that type 12 Astroquartz sewing thread (J. P. Stevens and CO.) be used for machine sewing the joints in the silica cloth and that types MF Al 12/300/7Z and MF-B1 25/270/2Z metallic filament threads (Groton Laboratories) be used to sew the joints in the wire reinforced asbestos.

REV. SYM. ___

5.1

- The conclusions which can be made from the results of this investigation are as follows:
 - 1. Machine sewing the joints in the wire reinforced asbestos with the metallic filament threads is unacceptable because those joints made per 60B20508 using the MF-A1-12/300/7Z thread did not meet the strength requirements of 60B32053. Also, it was impossible to machine sew with the MF-B1-25/270/2Z thread because its diameter was too large to permit it to be fed through the sewing machine.
 - 2. Machine sewing the silica cloth with type 12 astroquartz sewing thread will produce joints which meet the 60B20508 drawing requirements and the strength requirements of the 60B32053 acceptance specification.

5.3

5.3.1

Samples of wire reinforced asbestos cloth were cut so that joints could be made in which the warp threads were parallel for some of the joints and at 45° for the remainder to see if fabric thread orientation would have any effect during machine sewing of the joints. The first attempts at machine sewing these joints with the metallic filament threads were unsuccessful because the diameter of the MF-B1-25/270/2Z thread was too large and because of excessive breakage of the MF-A1-12/300/7Z thread. The thread breakage problem was solved by modifying the Pfaff sewing machine by replacing its 725 rpm 0.4 horsepower motor with a 500 rpm 0.5 horse power motor. All attempts at modifying the sewing machine to feed the large diameter filament thread were unsuccessful.

The sewn joints made with the MF-A1-12/300/7Z thread on the parallel warp material were tested for breaking strength at room temperature and after being subjected to the temperature cycle shown in Figure I or Figure II. The joints were made with both free ends of the thread knotted and with the free ends unknotted. The breaking strength results are shown in Table I.

While the 60B32053 acceptance specification requires room temperature breaking strength only for the asbestos joints, the elevated temperature tests were run to determine what effect the elevated temperatures would have upon the integrity of the metallic filaments. Visual examination of the joints after the elevated temperature cycles indicated near total deterioration of the filaments as evidenced by a charred appearance and by crumbling when the joints were flexed.

5.3.1 (Continued)

The room temperature breaking strengths of the metallic filament threads were determined and are shown in Table II. The 0.010 inch diameter Inconel wire which is currently being used for hand sewing the asbestos joints was tested and is included in Table I for comparison purposes.

Machine sewn joints were made in the high silica cloth using the type 12 astroquartz thread. The joints were made using the stitching specified in 60B20508 and tested for room temperature. breaking strength per 60B32053. An average breaking strength of 23 1b/in of width was obtained for the three samples tested. Since the individual values (20 1b/in, 24 1b/in, and 25 1b/in) as well as the average, were above the minimum of 18 1b/in required by 60B32053, machines sewing appears to be feasible for making the joints in the high silica cloth. The silica cloth joints were not tested at elevated temperature because the type 12 thread and the thread presently being used for hand sewing these joints are made of essentially the same material and the hand dewn joints have had no difficulty in surviving

the thermal environment expected for the curtain assembly.

PAGE

TABLE I

MACHINE SEWN WIRE REINFORCED ASBESTOS JOINTS

MF-A1-12/300/7Z THREAD

Minimum Acceptable Breaking Strength per 60B32053-250 lb/inch of width

1. Both ends of thread knotted

	Temperature	Breaking Strength lbs/inch of width
	Room Temperature After Figure I cycle After Figure II cycle	194 70 90
2.	Both ends of thread unknotted	
	Temperature	Breaking Stren gt h lbs/inch of width
	Room Temperature After Figure I cycle After Figure II cycle	115 105 86

REV. SYM. ___

TABLE II

SEWING THREAD ROOM TEMPERATURE BREAKING STRENGTH

Material	Breaking Strength (1bs)
MF-A1 12/300/7Z	1.44
Metallic Filament Thread	1.67
MF-B1 25/270/2Z	4.75
Metallic Filament Thread	5.00
0.010 inch Inconel wire	3.86
	4.18

REV. SYM. _

1800 1600 1400 1200 100d TEMPERATURE (%) 400 STREAGE TEMPERATURE 200 TIME TIME (STOONDS) CALC REVISED DATE T5-6556-10 FIGURE I CHECK ÁPR APR PAGE THE BOEING COMPANY

3 4013 8000

12

